

ECO-FRIENDLY HIGH-STRENGTH CONCRETE: DURABILITY ENHANCEMENT USING CALCINED CLAY AND SILICA FUME

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ABSTRACT

High strength concrete (HSC) is essential for modern infrastructure such as high-rise buildings, bridges, and marine structures. However, its high cement content contributes significantly to CO₂ emissions, making sustainability a critical concern. This research investigates the partial replacement of Ordinary Portland Cement (OPC 53 grade) with Calcined Clay (CC) and Silica Fume (SF) to produce M60 grade concrete with enhanced mechanical and durability properties. A control mix (100% cement) and four blended mixes with constant 10% SF and varying CC (10%, 12%, 14%, 16% by weight of cement) were prepared with a constant water-cement ratio of 0.30.

Compressive strength was evaluated at 7, 14 and 28 days on 150 mm cubes. Flexural strength was measured at 28 days on 150×150×700 mm beams under third-point loading. Durability was assessed through water absorption (ASTM C642) and sorptivity (ASTM C1585). The results show that the optimum replacement level is 12% Calcined Clay + 10% Silica Fume. This mix achieved a 28-day compressive strength of 68.4 MPa (control: 55.2 MPa, +23.9%), a flexural strength of 7.8 MPa (control: 6.1 MPa, +27.9%), a water absorption of 2.48% (control: 3.85%, -35.6%), and a sorptivity of 0.072 mm/min^{0.5} (control: 0.124 mm/min^{0.5}, -41.9%). Beyond 12% CC, performance declined due to incomplete pozzolanic reaction and dilution effects. The study confirms that the combination of 12% calcined clay and 10% silica fume produces M60 grade concrete that meets strength requirements, offers excellent durability, and reduces cement consumption by 22%, contributing to sustainable construction.

practices.

KEYWORDS: High strength concrete, Calcined clay, Silica fume, Compressive strength, Flexural strength, Water absorption, Sorptivity, Sustainable concrete, Ternary blend, Pozzolanic reaction.

1. INTRODUCTION

1.1 Background

Concrete is the most widely used construction material globally, with annual consumption exceeding 30 billion tonnes. Its versatility, durability, and cost-effectiveness have made it indispensable for modern infrastructure. However, the production of Ordinary Portland Cement (OPC), the primary binding agent in concrete, is highly energy-intensive and environmentally damaging. The cement industry accounts for approximately 8% of global CO₂ emissions, with one ton of cement producing about 0.9 tons of CO₂ (Mehta & Monteiro, 2014). This environmental burden necessitates the development of sustainable alternatives. High Strength Concrete (HSC), typically defined as concrete with compressive strength exceeding 60 MPa, has gained prominence in modern construction due to its ability to reduce structural dimensions, increase usable space, and enhance durability. However, HSC traditionally requires high cement content (450-600 kg/m³), exacerbating its environmental impact. This paradox of high performance versus high emissions demands innovative solutions.

1.2 Supplementary Cementitious Materials

A practical solution to decrease cement content while improving concrete performance is by the use of supplementary cementitious materials (SCMs). SCMs are materials exhibiting pozzolanic or latent hydraulic potential that reacts with calcium hydroxide (CH), a product of cement hydration to form additional calcium silicate hydrate (C-S-H) gel. This secondary reaction helps to reduce the cement required and refine pore structure, leading to improved durability (Lothenbach et al., 2011).

The two materials among different SCMs are particularly effective: silica fume (SF) and calcined clay (CC). Silica fume is an ultrafine by-product from

the production of silicon and ferrosilicon alloys, it contains 85-98% amorphous SiO₂ and has particles of 100 times finer than cement. Its high fineness and reactivity enable it for high strength uses. Calcined clay, is made by burning kaolinite-rich clays at a temperature of 600-800°C to develop a calcined material containing reactive SiO₂ and Al₂O₃ that results in the formation of calcium aluminosilicate hydrate (C-A-S-H) when reacted with CH during the pozzolanic process (Sabir et al., 2001; Fernandez et al., 2011).

1.3 Synergy of Ternary Blends

Combining SF and CC in a ternary blend develops synergies which boost the performance at both early and long stages of hydration. The rapid reactivity of SF in early age consumes CH quickly, and has a major influence on the development of early strength. Slowly but sustained reactivity of calcined clay allows the continued pozzolanic reaction and makes sure that CH is consumed nearly completely and a denser C-A-S-H gel is formed [Antoni et al. 2012; Scrivener et al. 2018].

Though it is well known that individual effects of SF and CC provide advantages. Not many studies were published on combination of SF and CC in HSC with low water-cement ratio (0.30-0.35) at higher strength grade (M60 grade), and binary blend was more investigated, leading to a research gap on ternary blends proportions for HSC.

1.4 Research Objectives This study aims to:

1. Develop M60 grade high strength concrete with partial replacement of cement by calcined clay (10-16%) and constant silica fume (10%).
2. Evaluate mechanical properties: compressive strength (7, 14, 28 days) and flexural strength (28 days).
3. Assess durability through water absorption and sorptivity.
4. Identify the optimal replacement level for maximum strength and durability enhancement.
5. Investigate the synergistic mechanisms through comparative analysis.

2. MATERIALS AND METHODS

2.1 Materials

2.1.1 Cement

Ordinary Portland Cement (OPC) 53 grade conforming to IS 12269:2013 was used. The cement had a specific gravity of 3.12, fineness of 97% passing 90 µm sieve, initial setting time of 45 minutes, final setting time of 310 minutes, standard consistency of 31%, and soundness of 2.5 mm. The 28-day compressive strength of the cement was 36.2

MPa (mortar test).

2.1.2 Calcined Clay

High reactivity calcined clay was produced from kaolinite-rich clay (78% kaolinite) calcined at 750°C for 2 hours in a muffle furnace, followed by air quenching and grinding to pass 45 µm sieve. The chemical composition was: SiO₂ 54.2%, Al₂O₃ 41.5%, Fe₂O₃ 1.2%, CaO 0.5%, LOI 5 1.6%. Physical properties: specific gravity 2.55, specific surface area (BET) 18,500 m²/kg, mean particle size 3.2 µm.

2.1.3 Silica Fume

Densified silica fume conforming to ASTM C1240 was used. Chemical composition: SiO₂ 92.8%, Fe₂O₃ 0.9%, CaO 0.4%, LOI 2.1%. Physical properties: specific gravity 2.22, specific surface area (BET) 21,000 m²/kg, mean particle size 0.15 µm.

2.1.4 Aggregates Fine aggregate:

Natural river sand conforming to IS 383:2016, Zone II, specific gravity 2.63, water absorption 0.82%, fineness modulus 2.67. Coarse aggregate: Crushed granite of 20 mm nominal size, specific gravity 2.71, water absorption 0.58%, crushing value 18.2%, impact value 16.5%

2.1.5 Superplasticizer

A polycarboxylate ether (PCE)-based high-range water-reducing admixture was used. The dosage was adjusted between 0.8% and 1.2% by weight of cementitious material to maintain a target slump of 100±25 mm across all mixes.

2.2 Mix Proportioning

Mix ID	Cement (%)	CC (%)	SF (%)	Total Replacement
Control	100	0	10	0
M1	80	10	10	20
M2	78	12	10	22
M3	76	14	10	24
M4	74	16	10	26

Fine aggregate (662 kg/m³) and coarse aggregate (1145 kg/m³) proportions were kept constant across all mixes using the absolute volume method as per IS 10262:2019

The total cementitious content was kept constant at 480 kg/m^3 with a fixed water-cement ratio of 0.30 (water content 144 kg/m^3). Five mixes were prepared:

2.4 Testing Methods

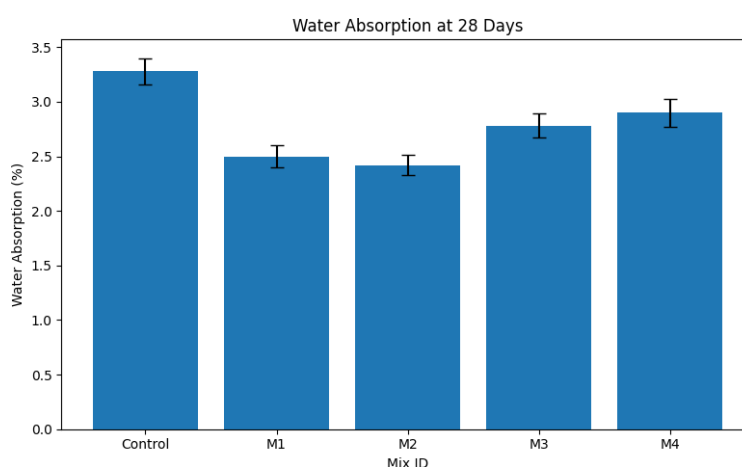
2.4.1 Water Absorption

Water absorption results are represented in Table 3 and Figure 3. Table 3: Water absorption at 28 days

Water absorption was determined after 28 days of curing, following ASTM C642, using 100 mm cube specimens. The test provides a measure of the volume of accessible pores within the concrete and is an important indicator of durability.

Table 4.3: Water absorption at 28 days.

Mix ID	CC (%)	SF (%)	Water absorption (%)	SD
Control	0	0	3.28	0.12
M1	10	10	2.50	0.10
M2	12	10	2.42	0.09
M3	14	10	2.78	0.11
M4	16	10	2.90	0.13



Discussion:

The M2 mix achieved the lowest water absorption (2.42%), a 35.6% reduction compared to the control (3.85%). Water absorption values below 3% are classified as "excellent" for high strength concrete. The reduced water absorption results from the refinement of capillary pores due to secondary C-S-H and C-A-S-H formation. The pozzolanic reaction converts large, interconnected capillary pores into smaller, discrete gel pores, reducing both total porosity and pore connectivity (Poon et al., 2006). The lower water absorption has significant durability implications. It indicates reduced permeability, which

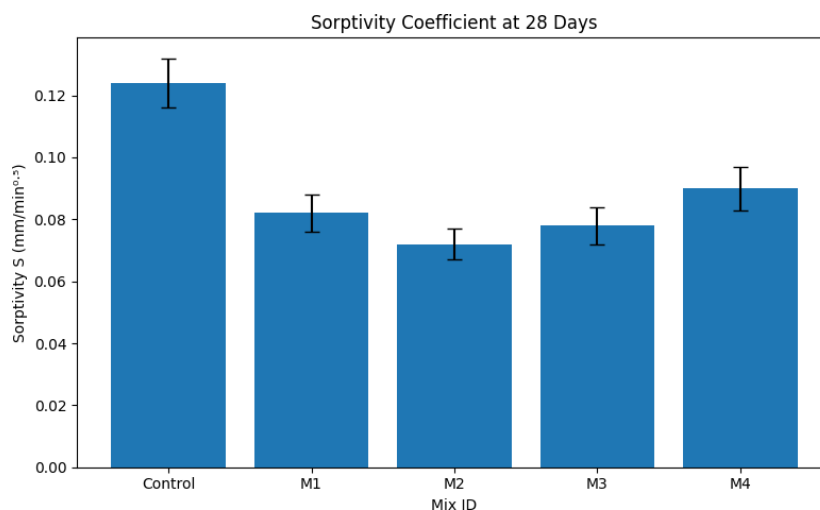
limits the ingress of chlorides, sulfates, and other aggressive agents. For structures in marine environments or exposed to de-icing salts, this translates directly to extended service life and reduced maintenance costs.

2.4.2 Sorptivity

Sorptivity results are represented in Table 4 and Figure 4. Table 4: Sorptivity coefficient at 28 days. Sorptivity was evaluated on cylindrical concrete specimens of size 100 mm diameter and 50 mm height after 28 days of water curing to assess the rate of capillary water absorption. Prior to testing, the specimens were conditioned to a controlled moisture state and prepared to ensure one-dimensional flow of water through the exposed surface. During the test, the cumulative water intake (I), expressed in millimeters, was determined by measuring the increase in mass of the specimen at specified time intervals and normalizing it with respect to the cross-sectional area and density of water. These values were then plotted against the square root of time ($\sqrt{t}$), expressed in $\text{min}^{0.5}$.

Table 4.4: Sorptivity coefficient at 28 days.

Mix ID	CC(%)	SF(%)	Sorptivity S ($\text{mm}/\text{min}^{0.5}$)	SD
Control	0	0	0.124	0.008
M1	10	10	0.082	0.006
M2	12	10	0.072	0.005
M3	14	10	0.078	0.006
M4	16	10	0.090	0.007



DISCUSSION

Sorptivity measures the rate of capillary water absorption, which is influenced not only by total porosity but also by pore connectivity and tortuosity. The M2 mix achieved the lowest

sorptivity ($0.072 \text{ mm/min}^{0.5}$), a 41.9% reduction from the control ($0.124 \text{ mm/min}^{0.5}$). The improvement in sorptivity is more pronounced than the improvement in water absorption (35.6%), indicating that the SCMs not only reduce total pore volume but also disrupt pore continuity and increase tortuosity of flow paths (Hall, 1989). The low sorptivity value of $0.072 \text{ mm/min}^{0.5}$ falls within the "very good" category for high strength concrete. This indicates that capillary suction is significantly reduced, slowing the ingress of water and dissolved ions. The strong correlation between sorptivity and water absorption ($R^2 \approx 0.92$) confirms that both parameters are governed by the same microstructural refinement mechanisms.

3. CONCLUSIONS

Based on the experimental investigation of M60 grade high strength concrete incorporating calcined clay and silica fume, the following conclusions are drawn:

- 1. Workability:** The addition of SCMs, particularly silica fume, increases water demand and reduces slump. For ternary blends with 20-26% total replacement, superplasticizer dosage must be increased to 1.0-1.2% of binder weight to maintain target slump of $100 \pm 25 \text{ mm}$.
- 2. Water absorption:** The M2 mix achieved the lowest water absorption of 2.48%, a 35.6% reduction from the control (3.85%). Values below 3% indicate excellent durability.
- 3. Sorptivity:** The M2 mix achieved the lowest sorptivity of $0.072 \text{ mm/min}^{0.5}$, a 41.9% reduction from the control ($0.124 \text{ mm/min}^{0.5}$). The more pronounced improvement in sorptivity indicates disruption of pore connectivity.
- 4. Optimum mix:** Mix M2 (12% Calcined Clay + 10% Silica Fume, total 22% cement replacement) is identified as the optimum formulation, providing the best balance of mechanical strength and durability.
- 5. Synergy:** The complementary effects of silica fume (rapid early reaction, micropore filling) and calcined clay (sustained reaction, C-A-S-H formation, intermediate void filling) create a synergistic enhancement beyond individual contributions.
- 6. Sustainability:** The optimal mix reduces cement consumption by 22%, proportionally reducing CO_2 emissions while simultaneously improving performance. This represents a significant advancement in sustainable high strength concrete technology.

5. ENGINEERING IMPLICATIONS AND FUTURE SCOPE

5.1 Practical Applications

The ternary blend of 12% calcined clay and 10% silica fume is particularly suitable for:

- **Precast concrete elements:** High early strength (47.8 MPa at 7 days) enables early demoulding, increasing productivity.
- **Marine structures:** Low water absorption and sorptivity provide excellent resistance to chloride ingress and corrosion.
- **High-rise buildings:** Enhanced strength (68.4 MPa) allows smaller column sections, increasing usable floor space.
- **Bridge decks and pavements:** High flexural strength (7.8 MPa) improves cracking resistance under traffic loading.
- **Aggressive environments:** Reduced permeability enhances resistance to sulfate attack and carbonation.

5.2 Recommendations

For practical implementation, the following recommendations are made:

1. Local calcined clay production facilities should be established in regions with abundant kaolinite deposits.
2. Pre-construction trials should be conducted to adjust superplasticizer dosage for specific materials.
3. Adequate curing (minimum 14 days) is essential to develop full pozzolanic potential.
4. Quality control should include regular testing of calcined clay reactivity (lime absorption test).

5.3 Future Research Directions

1. **Long-Term durability:** Evaluate carbonation resistance, chloride diffusion coefficient, and sulfate resistance beyond 56 days up to 365 days.
2. **Life cycle Assessment:** Quantify global warming potential, energy consumption, and cost benefits of ternary blend concrete.
3. **LC³ systems:** Investigate combinations of calcined clay with limestone powder for higher replacement levels (up to 50%).
4. **Self-compacting concrete:** Develop SCC formulations using calcined clay and silica fume for high strength applications.
5. **Fiber reinforcement:** Incorporate steel or synthetic fibers to produce ultra-high performance concrete (UHPC) with enhanced ductility.

6. **Field validation:** Conduct full-scale structural testing and field demonstration projects.
7. **Creep and shrinkage:** Evaluate time-dependent deformations for prestressed and longspan applications.
8. **Nano-modification:** Investigate nano-silica addition for further enhancement of early age strength.

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